



# The CONTACTOR™

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## SRU Thermal Oxidizer

**T**ail gas oxidation is the last processing step in an SRU before unrecoverable material and contaminants are discharged to the plant's stack, thence to atmosphere. This is where sulfur emissions are measured and compliance with emission regulations is assessed. Thermal oxidation is indeed the tail of the dog and it can end up wagging the dog.

The unit's purpose is to oxidize anything that will react with oxygen in a reasonable length of residence time so that what is discharged to the stack and the atmosphere is  $N_2$ ,  $CO_2$ , water vapor, and a very small amount of  $SO_2$ . Oxidizer performance is dictated by the three Ts: Time, Temperature, and Turbulence.

The oxidizer consists primarily of a burner and a reactor space or volume. A hydrocarbon fuel is burned with considerable excess air. The excess air is then partially consumed by various oxidation reactions in the reactor volume. The thermal reactor performs several important functions:

- Contaminant destruction;
- Dilution of emitted species with inert species to reduce the concentration of regulated compounds;
- VOC destruction;
- Conversion of potentially dangerous chemical species such as  $H_2S$  to a relatively safer ones such as  $SO_2$  before emitting to atmosphere;
- Energy recovery via waste heat boiler.

### Model

SulphurPro®'s model for the thermal incinerator is a hybrid of reaction kinetics for individual species and Gibbs Free Energy Minimization. It uses fundamental reaction kinetics for all reduced sulfur species (regulated), hydrogen, carbon monoxide, and ammonia. Gibbs Free Energy Minimization is applied to all remaining species for which reaction kinetics data are unavailable, for complex free radical and exotic species chemistry, and for the diversity of fuel gas sources.

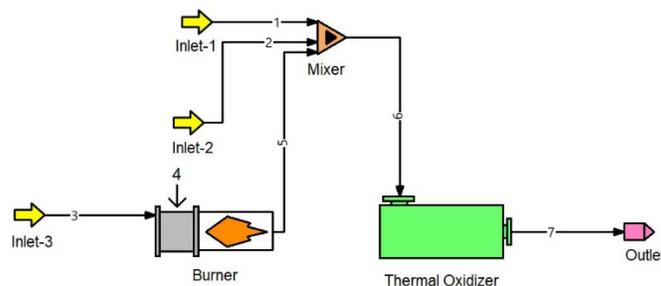
Design is often done using rules of thumb, without detailed models to support the approach, the calculations, or the design

itself. These and other factors provide ample motivation for model development, including:

- Opportunities for optimization. For example, optimization through saving fuel gas by combusting only what is required to drive the oxidation reactions to completion. This minimizes the free oxygen emanating from the thermal oxidizer, and it minimizes the size of the equipment necessary to meet emission regulations;
- Confidence in design. Design confidence can be improved by ensuring that contaminant destruction will take place to the extent desired (especially with CO where destruction is highly sensitive to residence time);
- Better accuracy. Greater accuracy can be had by kinetically modeling the oxidation of the most important species. This captures residence-time or space-velocity effects, which are not accounted for in an equilibrium or fractional-conversion type of model.

### Case Study

Figure 1 shows a typical Thermal Oxidizer arrangement with Burner, feed streams and Oxidizer. Inlet-1 is the



**Figure 1 Thermal Oxidizer with Feeds and Burner**

TGTU Contactor overhead, Inlet-2 is effluent from the sulfur pit degasser (containing air plus trace  $H_2S$ ,  $S_x$ , etc.), Inlet-3 is fuel gas for the burner (in this case, methane), and Stream 4 is 1 burner combustion air (130% of stoichiometric air required for combustion.)

The reactor data used in the simulation are its volume (5 m<sup>3</sup>) and its diameter (3 m) leaving the length calculated as 1.416 m. Reactions calculated by chemical kinetics require the reactor length to be divided into segments, in this case 10.

Species modeled kinetically include all reduced sulfur species (H<sub>2</sub>S, COS, CS<sub>2</sub>), H<sub>2</sub>, CO, NH<sub>3</sub> (with multiple competing pathways) together with all their assumed reaction products as shown in the dialog of Table 1. Other species (except Argon) are handled via Gibbs Free Energy Minimization, and all reactions are solved simultaneously. Gibbs components reach equilibrium in the first Oxidizer segment while kinetically controlled species continue to react throughout the reactor volume.

**Table 1 Kinetically Controlled Reactions**

Select All	Select None		Kinetic Factor	
<input checked="" type="checkbox"/>		H <sub>2</sub> S Oxidation	2H <sub>2</sub> S + 3O <sub>2</sub> <--> 2SO <sub>2</sub> + 2H <sub>2</sub> O	1.0
<input checked="" type="checkbox"/>		COS Oxidation	2COS + 3O <sub>2</sub> <--> 2CO <sub>2</sub> + 2SO <sub>2</sub>	1.0
<input checked="" type="checkbox"/>		CS <sub>2</sub> Oxidation	CS <sub>2</sub> + 3O <sub>2</sub> <--> CO <sub>2</sub> + 2SO <sub>2</sub>	1.0
<input checked="" type="checkbox"/>		H <sub>2</sub> Oxidation	2H <sub>2</sub> + O <sub>2</sub> <--> 2H <sub>2</sub> O	1.0
<input checked="" type="checkbox"/>		CO Oxidation	2CO + O <sub>2</sub> <--> 2CO <sub>2</sub>	1.0
<input checked="" type="checkbox"/>		Sour NH <sub>3</sub> Oxidation	2NH <sub>3</sub> + SO <sub>2</sub> <--> N <sub>2</sub> + 2H <sub>2</sub> O + H <sub>2</sub> S	1.0
<input checked="" type="checkbox"/>		NH <sub>3</sub> Oxidation	4NH <sub>3</sub> + 3O <sub>2</sub> <--> 6H <sub>2</sub> O + 2N <sub>2</sub>	1.0
<input checked="" type="checkbox"/>		NH <sub>3</sub> Decomposition	2NH <sub>3</sub> <--> N <sub>2</sub> + 3H <sub>2</sub>	1.0

Table 2 presents details of the vapor inlet stream to the thermal oxidizer, i.e., to Segment 1.

**Table 2 Details of Reactor Inlet Stream**

Temperature (°F)	1,386.025		
Pressure (psia)	14.700		
Mass Flow Rate (lb/h)	44,549.704		
Composition (mol%)			
Water	26.816	NH <sub>3</sub>	1.589e-07
CO <sub>2</sub>	4.286	SO <sub>2</sub>	3.203e-05
H <sub>2</sub>	1.832	C1	1.219e-08
O <sub>2</sub>	2.340	COS	3.437e-04
Ar	0.327	CS <sub>2</sub>	4.748e-07
S <sub>2</sub>	1.534e-03	CO	2.658e-02
S <sub>6</sub>	7.677e-06	N <sub>2</sub>	64.251
S <sub>8</sub>	7.923e-07	NO	0.114
MDEA	1.104e-05	NO <sub>2</sub>	8.791e-05
H <sub>2</sub> S	5.520e-03		

Table 3 shows the profile of species molar flow rates (lbmol/h) along the flow path of the thermal reactor

**Table 3 Species Flow Profiles (lbmol/h) along Reactor**

	From 1†	From 2	From 4	From 7	From 10
Water	497.16	497.16	497.16	497.16	497.16
CO <sub>2</sub>	74.82	74.82	74.82	74.82	74.82
H <sub>2</sub>	3.84e-3	4.46e-7	5.3e-15	4.3e-27	8.1e-40
O <sub>2</sub>	25.22	25.22	25.22	25.22	25.22
Ar	5.67	5.67	5.67	5.67	5.67
S <sub>2</sub>	0	0	0	0	0
S <sub>6</sub>	0	0	0	0	0
S <sub>8</sub>	0	0	0	0	0
MDEA	0	0	0	0	0
H <sub>2</sub> S	4.63e-5	2.16e-8	4.1e-15	2.2e-25	2.6e-38
NH <sub>3</sub>	1.17e-9	4.75e-13	6.9e-20	2.4e-30	2.8e-45
SO <sub>2</sub>	0.156	0.156	0.156	0.156	0.156
C1	0	0	0	0	0
COS	1.80e-5	5.26e-8	3.9e-13	5.1e-21	1.5e-29
CS <sub>2</sub>	1.21e-7	1.72e-9	3.0e-13	4.5e-19	1.6e-25
CO	3.35e-4	2.43e-7	1.0e-13	1.8e-23	7.4e-34
N <sub>2</sub>	1115.73	1115.73	1115.73	1115.73	1115.73
NO	6.36e-2	6.36e-2	6.36e-2	6.36e-2	6.36e-2
NO <sub>2</sub>	3.38e-4	3.38e-4	3.38e-4	3.38e-4	3.38e-4

This is a hybrid kinetic model that weds reaction kinetics for the species important in determining sulfur emissions with Gibbs Free Energy Minimization for non-critical species (and for which kinetic data are unavailable). No simulator other than SulphurPro® is capable of modeling a thermal oxidizer to this level of completeness and accuracy. It is certainly far more accurate than an equilibrium-only model or with assumed conversions. Note that kinetically determined species rapidly decline to immeasurably small values as they progress through the oxidizer. SO<sub>2</sub> is the only emergent sulfur species.

In the design phase, one can experiment with thermal oxidizer size, burner residual oxygen and temperature to ensure sufficient conversion of critically-restricted, permitted pollutants such as H<sub>2</sub>S, SO<sub>2</sub>, CO, etc. In operations, because SulphurPro's Thermal Oxidizer model is fully-predictive, it can be used to evaluate the effect of process changes (tail gas flow and composition, sweep and degassing feeds to the Oxidizer) with a high degree of reliability.

To learn more about this and other aspects of gas treating and sulphur recovery, plan to attend one of our training seminars. Visit [www.protreat.com/seminars](http://www.protreat.com/seminars) for details.

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† From 1 indicates From Segment 1 (at front of Oxidizer). From 10 means Oxidizer effluent.